



Kabier Salam LLFA Engineer

11 11 2022

Dear Kabier,

Application no: 22/02470/DISC

Location: OS Parcels 3309 And 4319 Adjoining And North Of, Milton Road, Adderbury

Re: [0202] Land North Of Milton Road, Adderbury

Following you comments regarding drainage. We respond to your queries below.

#### **Condition 9 states:**

"No development shall commence unless and until full design details of the proposal, implementation, maintenance and management of a surface water drainage scheme have been submitted to and approved in writing by the local planning authority. Those details shall include:"

**Query a:** "Information about the design storm period and intensity (1 in 30 & 1 in 100 (+40% allowance for climate change), discharge rates and volumes (both pre and post development), temporary storage facilities, means of access for maintenance, the methods employed to delay and control surface water discharged from the site, and the measures taken to prevent flooding and pollution of the receiving groundwater and/or surface waters;

Provide detailed drainage drawing to show all drainage infrastrucure and SuDS. Ensure invert and cover levels has been provided. Provide surface water catchment plan, showing the extent of the impermeable area and stating the area. The detailed drainage strategy should also show phase 1 and its proposals."

**Response:** See attached proposed site layouts including catchment areas and full set of calculations.

**Query b:** "Any works required off-site to ensure adequate discharge of surface water without causing flooding or pollution (which should include refurbishment of existing culverts and headwalls or removal of unused culverts where relevant)"

**Response:** All flows are kept on site. No changes to outside infrastructure are required.

**Query c:** "Flood water exceedance routes, both on and off site; Provide exceedance plan, showing surface water run off by using flow arrows. Ensure all surface water is kept away from structures and within the site boundary."





**Response:** The exceedance flow routes are provided on the main site layout. No risk to proposed or existing buildings.

**Query d:** "A timetable for implementation;

Not provided."

**Response:** Due to the community nature of the development the timescales could fluctuate depending on the grants and the moneys collected by the community. The development will be implemented as follows:

Stage 1: Winter 2022 and Spring 2023

Stage 2: Spring 2023 and Summer 2023

**Query e:** "Site investigation and test results to confirm infiltrations rates. Infiltration testing location plan not provided. Reason - To ensure satisfactory drainage of the site in the interests of public health, to avoid flooding of adjacent land and property and to comply with Policy ESD6 of the Cherwell Local Plan 2011 – 2031 Part 1, Saved Policy ENV1 of the Cherwell Local Plan 1996 and Government guidance contained within the National Planning Policy Framework."

**Response:** See attached updated site plan showing the location of the trial pits and their results. The calculations have been undated with the new soakaway results.

Argemiro Rivera
Director
arge@rida-reports.co.uk





# Drainage Design





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Drawing Scale Bar Drawing Line Scale Length Scale Length Scale Length Scale Length Scale Length

1:5 = 0.25 metres 1:200 = 10.0 metres
1:10 = 0.5 metres 1:250 = 12.5 metres
1:20 = 1.0 metres 1:500 = 25.0 metres
1:25 = 1.25 metres 1:1000 = 50.0 metres
1:50 = 2.5 metres 1:1250 = 62.5 metres
1:100 = 5.0 metres 1:2500 = 125 metres
Measure length of line above for checking of scale

# GENERAL NOTES

- 1. All dimensions are in millimetres and levels in m AOD unless stated otherwise.
- 2. Do not scale. If in any doubt, consult Engineer.
- 3. Read in conjunction with the architects and engineers schedule drawings.
- 4. Check inverts and sizes of existing pipes prior to the commencement of any work. Report any discrepancies
- to the engineer and await instructions. 5. The location of services is shown as indicative. This
- drawing should be read in conjunction with the utilities drawings. No warranty to their accuracy can be given. The contractor shall take all necessary measures to satisfy himself as to the location of the existing services and connection points. Excavation should be undertaken in compliance with HSG47.
- 6. Concrete structures design sulphate class and ACEC concrete class unknown.
- 7. Pipework to be 110mm Thermoplastics U-PVC (Polypipe or similar) installed at levels marked on this drawing. Pipe bedding should be class Z in pipes within 1.5m of the building or shallower than 700mm below ground level. For all other areas the pipe bedding should be class S.
- 8. Joints and fittings for gravity sewers shall comply with the relevant provisions of BS EN 1401-1, BS EN 1852 and BS EN 12666-1. Pipes shall have a limit of 6% deformation. Pipes shall be SN8 ring stiffness and stamped accordingly. Pipe sections shall not be longer
- 9. Plastic chambers and rings, including demarcation chambers, shall comply with BS EN 3598-1 or BS EN 13598-2 as appropriate.
- 10. Inspection chamber covers and frames shall comply with the relevant provisions of BS EN 124 and should be
- 11. All inspection chamber covers shall be the non-ventilating type and shall have closed keyways.
- 12. Testing of pipelines should be as follow:
- Gravity Pipework: Air pipe testing. Pipework should withstand a pressure of 100mm water gauge and this should not fall by more than 25mm in a 5minute period. However where traps or gullies are connected they should withstand a pressure of 50mm water gauge and this should not fall by more than 12mm in a 5minute period. It is recommended that pipework installations are tested in sections rather than waiting to complete in one operation.
- 13. Manhole covers to be set square to the building. Covers of existing manholes to be adjusted to match final ground levels.
- 14. Granular Bedding for pipes shall be constructed by spreading and compacting granular bedding material over the full width of the pipe trench. After the pipes have been laid, additional granular material shall, if required, be placed and compacted equally on each side of the pipes and, where practicable, this shall be done in sequence with the removal of the trench supports.



Drawing Status: **PRELIMINARY** 



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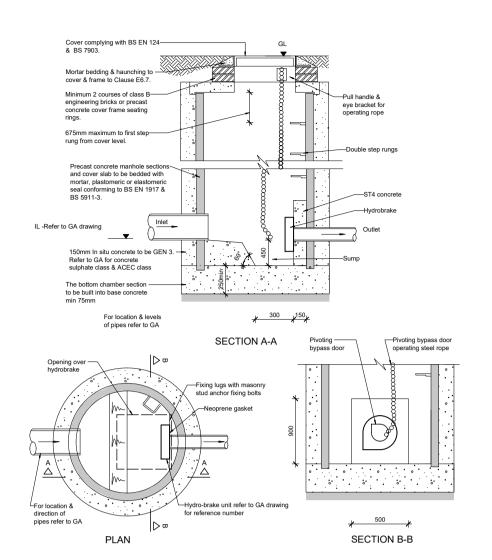
Land North Of Milton Road, Adderbury

Proposed Drainage Strategy Phase 1 and 2

0202

003

P1

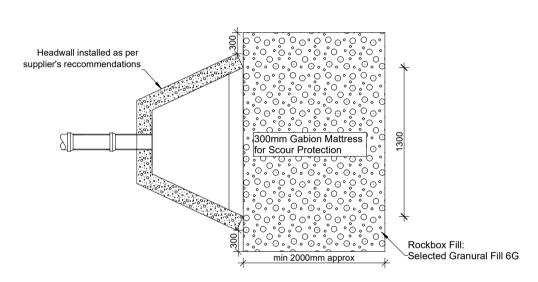


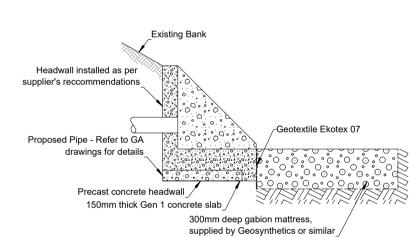
NOTE:

1. Refer to GA for manhole size and Hydrobrake reference number

2. Hydrobrake to be installed as per supplier's recommendations

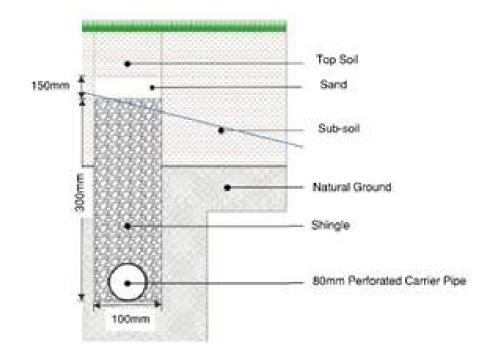
#### Flow Control Device Chamber- Hydrobrake

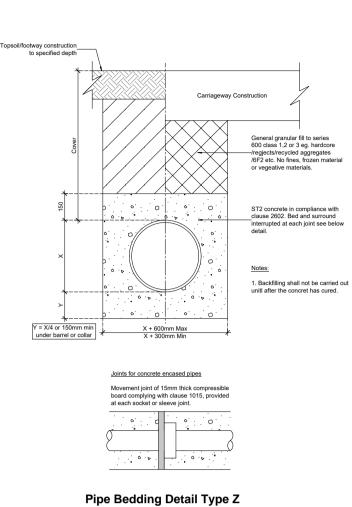


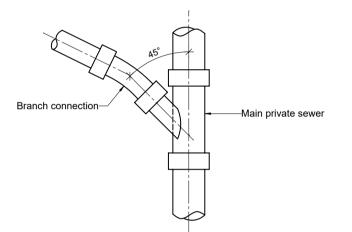


Headwall	Accommod ate Pipe Sizes	Back wall height (external)	Front wall height (external)	Width at back wall (internal)	Width at front wall (internal)	Headwall Length	Wall Thickness	Floor thickness	Approx. Weight
	mm	mm	mm	mm	mm	mm	mm	mm	kg
FPMcCann Precast Headwall HW Small	300,225,160	810	300	520	1300	1320	100	162	1090

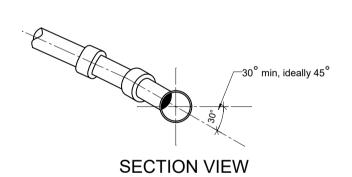
Precast Concrete Headwall







**PLAN VIEW** 



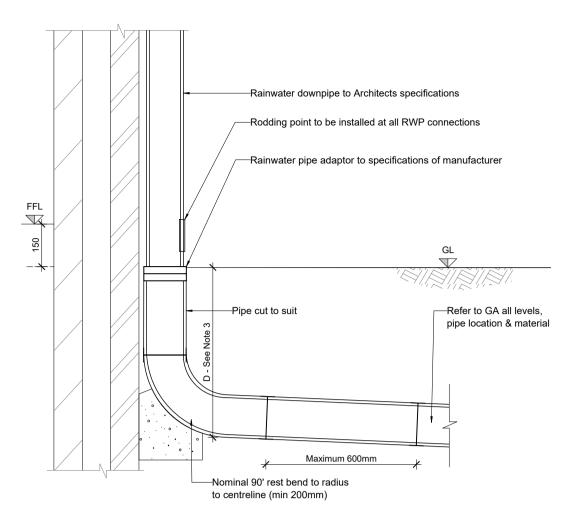
NOTES:

1. The vertical angle between the connecting pipe and the horizontal should be greater than 0° and not more than 60°.

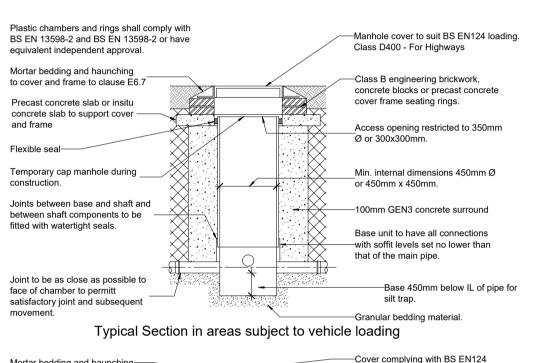
2. Where the connection is being made to a sewer with a nominal internal diameter of 300 mm or less, connections should be made using 45° angle, or 90° angle, curved square junctions.

3. Connections made with junction fittings should be made by cutting the existing pipe, inserting the junction fitting and jointing with flexible repair couplings or slip couplers.

# Lateral Connection to private sewer



8251 - External Rainwater Pipe Connection Detail

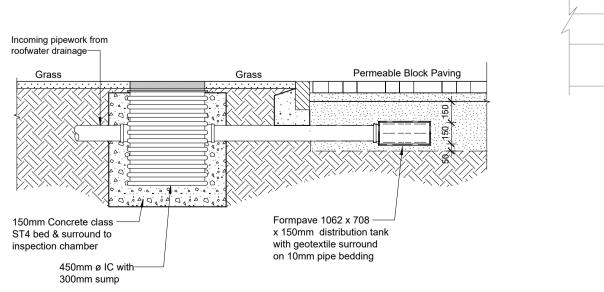


Mortar bedding and haunching——— to cover and frame to clause E6.7		Class B125 - For Driveways, Footways and Landscaping Areas
150mm deep concrete collar———		
Temporary cap shaft during construction		——Access opening restricted
Min. internal dimensions 450mm Ø_ or 450mm x 450mm.		refer to manhole schedule —Type 1 sub base (thickness varies). —Flexible Seal.
Sited	l in domestic driveways or foc	otways
		Cover and frame to BS EN124

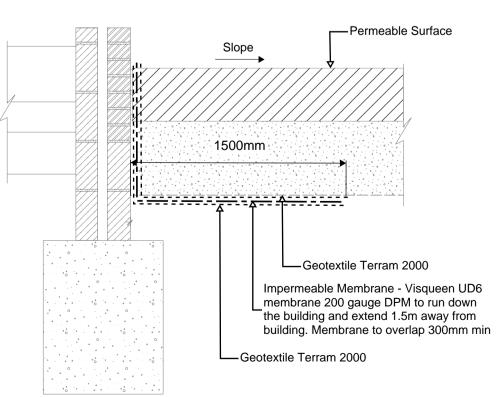
lortar bedding and haunching		<u>/</u>	Class A15 - For Gardens
o cover and frame to clause E6.7	<del>\</del>		—Topsoil
Temporary cap shaft during			—Access opening restricted.
construction	××		Refer to manhole schedule
			for details
Min. internal dimensions 450mm Ø_	$\longrightarrow$	—'III <del>-                                  </del>	—Type 1 sub base (thickness varies).
or 450mm x 450mm.	$\times$	<u></u> ∦ : KX_	
	V		
Site	ed in private gar	den - No loadir	ng

# Notes: 1. Refer to drawing 8193 for base layouts.

Silt Trap Plastic



SD064 - Sump and Dispersion Unit



Permeable Surface Against Building

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Drawing Scale Bar

Drawing Line Drawing Line length

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Measure length of line above for checking of scale

GENERAL NOTES



PRELIMINARY



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Client:

Land North Of Milton Road, Adderbury

Drawing:

Standard Details

Print Size: Project No: Drawing No: Rev A1 0202 006

File: Land North Of Milton Roa Network: Storm

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#### **Design Settings**

Rainfall Methodology FSR Return Period (years) 2 Additional Flow (%) 0

FSR Region England and Wales

M5-60 (mm) 20.000 Ratio-R 0.409 CV 0.750

Time of Entry (mins) 6.00

Maximum Time of Concentration (mins) 30.00

Maximum Rainfall (mm/hr) 50.0

Minimum Velocity (m/s) 1.00

Connection Type Level Inverts

Minimum Backdrop Height (m) 0.200

Preferred Cover Depth (m) 0.500
Include Intermediate Ground 
✓
Enforce best practice design rules 
✓

#### **1 STANDARD Link Type**

Shape Circular Auto Increment (mm) 75
Barrels 1 Follow Ground x

#### **Available Diameters (mm)**

100 150

#### **Nodes**

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
Building	0.055	6.00	100.000	450	-79.325	595.400	0.400
Car Park	0.035	6.00	100.000	450	-69.325	595.449	0.500
OUT			100.000	450	-59.325	595.400	0.600

#### <u>Links</u>

Name	US	DS	Length	ks (mm) /	US IL	DS IL	Fall	Slope	Dia	T of C	Rain
	Node	Node	(m)	n	(m)	(m)	(m)	(1:X)	(mm)	(mins)	(mm/hr)
1.000	Building	Car Park	10.000	0.600	99.600	99.500	0.100	100.0	225	6.13	50.0
1.001	Car Park	OUT	10.000	0.600	99.500	99.400	0.100	100.0	100	6.34	50.0

Name	Vel	Сар	Flow	US	DS	Σ Area	Σ Add
	(m/s)	(I/s)	(I/s)	Depth	Depth	(ha)	Inflow
				(m)	(m)		(I/s)
1.000	1.307	52.0	7.5	0.175	0.275	0.055	0.0
1.001	0.769	6.0	12.2	0.400	0.500	0.090	0.0

#### **Pipeline Schedule**

Link	Length (m)	Slope (1:X)	-	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
1.000	10.000	100.0	225	1 STANDARD	100.000	99.600	0.175	100.000	99.500	0.275
1.001	10.000	100.0	100	1 STANDARD	100.000	99.500	0.400	100.000	99.400	0.500

Link	US	Dia	Node	MH	DS	Dia	Node	MH
	Node	(mm)	Type	Type	Node	(mm)	Type	Type
1.000	Building	450	Manhole	1 STANDARD	Car Park	450	Manhole	1 STANDARD
1.001	Car Park	450	Manhole	1 STANDARD	OUT	450	Manhole	1 STANDARD

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**Node Car Park Online Pump Control** 

Flap Valve x Replaces Downstream Link Invert Level (m) 99.500

Design Depth (m) 0.500 Design Flow (I/s) 0.1 Switch on depth (m) 0.500 Switch off depth (m) 0.010

Depth Flow Depth Flow (m) (I/s) (m) (I/s) 0.001 0.000 0.500 0.000

**Node Car Park Carpark Storage Structure** 

Base Inf Coefficient (m/hr) 0.18450 Side Inf Coefficient (m/hr) 0.18450 Safety Factor 2.0 Porosity 0.30

Invert Level (m) 99.500 Time to half empty (mins) 12 Width (m) 70.000 Length (m) 10.000

400.0 Slope (1:X) Depth (m) 0.400

Inf Depth (m)

#### **Rainfall**

Event	Peak Intensity	Average Intensity	Event	Peak Intensity	Average Intensity
	(mm/hr)	(mm/hr)		(mm/hr)	(mm/hr)
1 year 15 minute summer	110.333	31.220	2 year 240 minute winter	14.914	5.932
1 year 15 minute winter	77.427	31.220	2 year 360 minute summer	17.054	4.389
1 year 30 minute summer	71.731	20.297	2 year 360 minute winter	11.086	4.389
1 year 30 minute winter	50.337	20.297	2 year 480 minute summer	13.385	3.537
1 year 60 minute summer	48.435	12.800	2 year 480 minute winter	8.893	3.537
1 year 60 minute winter	32.179	12.800	2 year 600 minute summer	10.937	2.992
1 year 120 minute summer	29.920	7.907	2 year 600 minute winter	7.473	2.992
1 year 120 minute winter	19.878	7.907	2 year 720 minute summer	9.733	2.609
1 year 180 minute summer	23.067	5.936	2 year 720 minute winter	6.541	2.609
1 year 180 minute winter	14.994	5.936	2 year 960 minute summer	7.979	2.101
1 year 240 minute summer	18.307	4.838	2 year 960 minute winter	5.286	2.101
1 year 240 minute winter	12.162	4.838	2 year 1440 minute summer	5.779	1.549
1 year 360 minute summer	14.012	3.606	2 year 1440 minute winter	3.884	1.549
1 year 360 minute winter	9.108	3.606	30 year 15 minute summer	270.732	76.608
1 year 480 minute summer	11.040	2.918	30 year 15 minute winter	189.988	76.608
1 year 480 minute winter	7.335	2.918	30 year 30 minute summer	175.606	49.690
1 year 600 minute summer	9.050	2.475	30 year 30 minute winter	123.232	49.690
1 year 600 minute winter	6.184	2.475	30 year 60 minute summer	116.589	30.811
1 year 720 minute summer	8.075	2.164	30 year 60 minute winter	77.459	30.811
1 year 720 minute winter	5.427	2.164	30 year 120 minute summer	70.174	18.545
1 year 960 minute summer	6.650	1.751	30 year 120 minute winter	46.622	18.545
1 year 960 minute winter	4.405	1.751	30 year 180 minute summer	52.993	13.637
1 year 1440 minute summer	4.848	1.299	30 year 180 minute winter	34.447	13.637
1 year 1440 minute winter	3.258	1.299	30 year 240 minute summer	41.313	10.918
2 year 15 minute summer	142.607	40.353	30 year 240 minute winter	27.448	10.918
2 year 15 minute winter	100.075	40.353	30 year 360 minute summer	30.933	7.960
2 year 30 minute summer	92.106	26.063	30 year 360 minute winter	20.107	7.960
2 year 30 minute winter	64.636	26.063	30 year 480 minute summer	24.064	6.359
2 year 60 minute summer	61.301	16.200	30 year 480 minute winter	15.988	6.359
2 year 60 minute winter	40.727	16.200	30 year 600 minute summer	19.523	5.340
2 year 120 minute summer	37.296	9.856	30 year 600 minute winter	13.339	5.340
2 year 120 minute winter	24.778	9.856	30 year 720 minute summer	17.268	4.628
2 year 180 minute summer	28.484	7.330	30 year 720 minute winter	11.605	4.628
2 year 180 minute winter	18.515	7.330	30 year 960 minute summer	14.015	3.690
2 year 240 minute summer	22.448	5.932	30 year 960 minute winter	9.284	3.690





File: Land North Of Milton Roa

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#### **Rainfall**

Event	Peak	Average	Event	Peak	Average
	Intensity	Intensity		Intensity	Intensity
	(mm/hr)	(mm/hr)		(mm/hr)	(mm/hr)
30 year 1440 minute summer	9.998	2.680	100 year 240 minute winter	35.822	14.249
30 year 1440 minute winter	6.719	2.680	100 year 360 minute summer	40.132	10.327
30 year +40% CC 15 minute summer	379.025	107.251	100 year 360 minute winter	26.087	10.327
30 year +40% CC 15 minute winter	265.983	107.251	100 year 480 minute summer	31.099	8.219
30 year +40% CC 30 minute summer	245.848	69.567	100 year 480 minute winter	20.662	8.219
30 year +40% CC 30 minute winter	172.525	69.567	100 year 600 minute summer	25.151	6.879
30 year +40% CC 60 minute summer	163.225	43.136	100 year 600 minute winter	17.185	6.879
30 year +40% CC 60 minute winter	108.443	43.136	100 year 720 minute summer	22.187	5.946
30 year +40% CC 120 minute summer	98.244	25.963	100 year 720 minute winter	14.911	5.946
30 year +40% CC 120 minute winter	65.271	25.963	100 year 960 minute summer	17.929	4.721
30 year +40% CC 180 minute summer	74.190	19.092	100 year 960 minute winter	11.876	4.721
30 year +40% CC 180 minute winter	48.225	19.092	100 year 1440 minute summer	12.706	3.405
30 year +40% CC 240 minute summer	57.839	15.285	100 year 1440 minute winter	8.539	3.405
30 year +40% CC 240 minute winter	38.427	15.285	100 year +40% CC 15 minute summer	492.044	139.231
30 year +40% CC 360 minute summer	43.306	11.144	100 year +40% CC 15 minute winter	345.294	139.231
30 year +40% CC 360 minute winter	28.150	11.144	100 year +40% CC 30 minute summer	321.827	91.066
30 year +40% CC 480 minute summer	33.690	8.903	100 year +40% CC 30 minute winter	225.843	91.066
30 year +40% CC 480 minute winter	22.383	8.903	100 year +40% CC 60 minute summer	214.603	56.713
30 year +40% CC 600 minute summer	27.332	7.476	100 year +40% CC 60 minute winter	142.577	56.713
30 year +40% CC 600 minute winter	18.675	7.476	100 year +40% CC 120 minute summer	129.111	34.120
30 year +40% CC 720 minute summer	24.175	6.479	100 year +40% CC 120 minute winter	85.778	34.120
30 year +40% CC 720 minute winter	16.247	6.479	100 year +40% CC 180 minute summer	97.196	25.012
30 year +40% CC 960 minute summer	19.621	5.167	100 year +40% CC 180 minute winter	63.180	25.012
30 year +40% CC 960 minute winter	12.997	5.167	100 year +40% CC 240 minute summer	75.485	19.949
30 year +40% CC 1440 minute summer	13.997	3.751	100 year +40% CC 240 minute winter	50.151	19.949
30 year +40% CC 1440 minute winter	9.407	3.751	100 year +40% CC 360 minute summer	56.184	14.458
100 year 15 minute summer	351.460	99.451	100 year +40% CC 360 minute winter	36.521	14.458
100 year 15 minute winter	246.639	99.451	100 year +40% CC 480 minute summer	43.539	11.506
100 year 30 minute summer	229.876	65.047	100 year +40% CC 480 minute winter	28.926	11.506
100 year 30 minute winter	161.317	65.047	100 year +40% CC 600 minute summer	35.212	9.631
100 year 60 minute summer	153.288	40.510	100 year +40% CC 600 minute winter	24.059	9.631
100 year 60 minute winter	101.841	40.510	100 year +40% CC 720 minute summer	31.062	8.325
100 year 120 minute summer	92.222	24.372	100 year +40% CC 720 minute winter	20.875	8.325
100 year 120 minute winter	61.270	24.372	100 year +40% CC 960 minute summer	25.100	6.610
100 year 180 minute summer	69.425	17.866	100 year +40% CC 960 minute winter	16.627	6.610
100 year 180 minute winter	45.128	17.866	100 year +40% CC 1440 minute summer	17.789	4.768
100 year 240 minute summer	53.918	14.249	100 year +40% CC 1440 minute winter	11.955	4.768

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Network: Storm Mario Mora 19/10/2022

Results for 1 year Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	Building	10	99.667	0.067	7.1	0.1946	0.0000	OK
15 minute winter	Car Park	14	99.521	0.021	11.7	1.9168	0.0000	OK
15 minute summer	OUT	1	99.400	0.000	0.0	0.0000	0.0000	ОК

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	Building	1.000	Car Park	7.2	1.388	0.138	0.0565	
15 minute winter	Car Park	Pump	OUT	0.0				0.0
15 minute winter	Car Park	Infiltration		7.6				

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Network: Storm Mario Mora 19/10/2022

#### Results for 2 year Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
		,	` '	` '		- ( /	` '	
15 minute winter	Building	10	99.676	0.076	9.2	0.2213	0.0000	OK
15 minute winter	Car Park	14	99.526	0.026	15.2	2.7887	0.0000	OK
15 minute summer	OUT	1	99.400	0.000	0.0	0.0000	0.0000	ОК

<b>Link Event</b>	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	Building	1.000	Car Park	9.3	1.477	0.179	0.0682	
15 minute winter	Car Park	Pump	OUT	0.0				0.0
15 minute winter	Car Park	Infiltration		9.2				

File: Land North Of Milton Roa Page 6 Network: Storm

Mario Mora 19/10/2022

#### Results for 30 year Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
	Noue	(1111113)	(111)	(111)	(1/3)	voi (iii <i>)</i>	(111 /	
15 minute winter	Building	10	99.706	0.106	17.5	0.3087	0.0000	OK
15 minute winter	Car Park	14	99.543	0.043	28.7	6.4354	0.0000	OK
15 minute summer	OUT	1	99.400	0.000	0.0	0.0000	0.0000	ОК

<b>Link Event</b>	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	Building	1.000	Car Park	17.7	1.717	0.340	0.1093	
15 minute winter	Car Park	Pump	OUT	0.0				0.0
15 minute winter	Car Park	Infiltration		15.5				

File: Land North Of Milton Roa Page 7 Network: Storm

Mario Mora 19/10/2022

13/10/2022

#### Results for 30 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US	Peak	Level	Depth	Inflow	Node	Flood	Status
	Node	(mins)	(m)	(m)	(I/s)	Vol (m³)	(m³)	
15 minute winter	Building	10	99.727	0.127	24.5	0.3689	0.0000	OK
15 minute winter	Car Park	15	99.559	0.059	40.3	9.9441	0.0000	OK
15 minute summer	OUT	1	99.400	0.000	0.0	0.0000	0.0000	OK

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	Building	1.000	Car Park	24.7	1.840	0.475	0.1412	
15 minute winter	Car Park	Pump	OUT	0.0				0.0
15 minute winter	Car Park	Infiltration		18.1				

File: Land North Of Milton Roa

Network: Storm Mario Mora 19/10/2022 Page 8

#### Results for 100 year Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
15 minute winter	Building	10	99.722	0.122	22.7	0.3540	0.0000	OK
15 minute winter	Car Park	15	99.555	0.055	37.4	8.9071	0.0000	OK
15 minute summer	OUT	1	99.400	0.000	0.0	0.0000	0.0000	ОК

<b>Link Event</b>	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	Building	1.000	Car Park	22.9	1.812	0.440	0.1331	
15 minute winter	Car Park	Pump	OUT	0.0				0.0
15 minute winter	Car Park	Infiltration		18.1				

File: Land North Of Milton Roa Page 9 Network: Storm

Mario Mora 19/10/2022

#### Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
4		,	(/	` '		- ( /	<b>(</b> )	011
15 minute winter	Building	10	99.746	0.146	31.8	0.4256	0.0000	OK
30 minute winter	Car Park	24	99.583	0.083	43.0	14.8337	0.0000	OK
15 minute summer	OUT	1	99.400	0.000	0.0	0.0000	0.0000	ОК

Link Event	US	Link	DS	Outflow	Velocity	Flow/Cap	Link	Discharge
(Upstream Depth)	Node		Node	(I/s)	(m/s)		Vol (m³)	Vol (m³)
15 minute winter	Building	1.000	Car Park	32.0	1.926	0.616	0.1733	
30 minute winter	Car Park	Pump	OUT	0.0				0.0
30 minute winter	Car Park	Infiltration		18.2				



# Soakaway Tests



Soakaway trial Pit 3 0.7m wide x 1.5m length x 1.0m deep Soakaway trial Pit 1 0.7m wide x 1.5m length x 1.0m deep Gower House Sycamore House Maple House Sundial House Cattle 103.9m Balancing Pond

Do not scale from this drawing. Refer to figured dimensions only. RIDA Reports Ltd registered in England and Wales No. 10590566. This drawing is copyright of RIDA Reports Ltd.

Drawing Scale Bar

| Drawing Line | Scale | Line |

GENERAL NOTES

This drawing should be read



PRELIMINARY



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Scale 1:500

Client:

Land North Of Milton Road, Adderbury

Trial Pit Layout

man n Layout

Print Size: Project No: Drawing No:

A1 0202 001

No: Revision: P1

Project:	Land North Of Milton Road, Adderbury	
Calculation By:	Mario Mora	
Title :	Soakaway Calculation	RIVA
Date:	19/10/2022	

#### TEST 1

Pit Dimensions:

L: 1500 mm W: 700 mm D: 1000 mm Key
Input
Calculation

Mean Surface Area
Depth of water
Time at 25% or at

2.85 m2 818 mm 204.5 mm of water Interpolating Values

Time	Water Depth
30	295
40	190
20.62	min From interpolat

t: 38.62 min. From interpolating values

Time

Time at 75% or at 613.5 mm of water
Interpolating Values
Time Water Depth

0 818
10 568
t: 8.18 min. From interpolating values

Volume of test Pit between 25% and 75% of water depth: 0.429 m3

Time Taken to drain between 25% and 75% of water depth: 30.44 min or 0.507 hr

**Test 1 - Soil Infiltration rate:** 

8.25E-05 m/s 0.29706 m/hr

# TEST 2

#### **Pit Dimensions:**

L: 1500 mm W: 700 mm D: 1000 mm

Key	
	Input
	Calculation

54.2 min. From interpolating values

Time		
Since Start	Water Level from GL	Depth of water
min	mm	mm
0	171	829
10	405	595
20	543	457
30	652	348
40	713	287
50	781	219
60	809	191
70	846	154

Mean Surface Area	2.87	m2
Depth of water	829	mm
Time at 25% or at	207.3	mm of water
	Interpola	ating Values
	Time	Water Depth
	50	219
	60	191

Time at 75% or at 621.8 mm of water
Interpolating Values
Time Water Depth

0 829
10 595
t: 8.857 min. From interpolating values

Volume of test Pit between 25% and 75% of water depth: 0.435 m3

Time Taken to drain between 25% and 75% of water depth: 45.34 min or

**0.756** hr

**Test 2 - Soil Infiltration rate:** 

5.57E-05 m/s 0.20042 m/hr

#### TEST 3

#### **Pit Dimensions:**

L: 1500 mm W: 700 mm D: 1000 mm

Key	,
	Input
	Calculation

Mean Surface Area Depth of water Time at 25% or at

2.88 m2 mm
207.5 mm of water Interpolating Values

	Time	Water Dept	h
	50	231	
	60	202	
:	58.1	min. From int	terpolating values

Time at 75% or at 622.5 mm of water

Interpolating Values

Time	Water Depth
0	830
10	595

t: 8.83 min. From interpolating values

Time Since Start	Water Level from GL	Depth of water
min	mm	mm
0	170	830
10	405	595
20	536	464
30	650	350
40	707	293
50	769	231
60	798	202
70	823	177
80	849	151
90	875	125
100	902	98

Volume of test Pit between 25% and 75% of water depth: Time Taken to drain between 25% and 75% of water depth:

**0.436** m3 **49.27** min or

**0.821** hr

Test 3 - Soil Infiltration rate:

5.12E-05 m/s 0.18450 m/hr

**SOAKAWAY TRIAL PIT 1 INFILTRATION RATE** 

5.12E-05 m/s 0.18450 m/hr

Project:	Land North Of Milton Road, Adderbury	
Calculation By:	Mario Mora	
Title :	Soakaway Calculation	RIVA
Date:	19/10/2022	

#### TEST 1

Pit Dimensions:

L: 1500 mm W: 700 mm D: 1000 mm Key Input Calculation

Time Since Start	Water Level from GL	Depth of water
min	mm	mm
0	197	803
10	487	513
20	693	307
30	824	176
40	981	19
50	1000	0

Mean Surface Area	2.82	m2	
Depth of water	803	mm	
Time at 25% or at	200.8	mm of wate	er
'	Interpola	ating Values	
	Time	Water Dept	h
	20	307	
	30	176	
t:	28.11	min. From in	terpolating values

Time at 75% or at 602.3 mm of water
Interpolating Values
Time Water Depth

0 803
10 513
t: 6.922 min. From interpolating values

m/s

m/hr

Volume of test Pit between 25% and 75% of water depth: 0.422 m3

Time Taken to drain between 25% and 75% of water depth: 21.19 min or 0.353 hr

Test 1 - Soil Infiltration rate: 1.18E-04 0.42384

# TEST 2

#### **Pit Dimensions:**

L: 1500 mm W: 700 mm D: 1000 mm

Key	
	Input
	Calculation

Time Since Start	Water Level from GL	Depth of water
min	mm	mm
0	181	819
10	476	524
20	660	340
30	781	219
40	911	89
50	1000	0

Mean Surface Area	2.85	m2			
Depth of water	819	mm			
Time at 25% or at	204.8	mm of wate	er		
Interpolating Values					
	Time	Water Dept	h		
	30	219			
	40	89			
t:	31.1	min. From in	terpolating values		

Time at 75% or at 614.3 mm of water
Interpolating Values
Time Water Depth

0 819
10 524
t: 6.941 min. From interpolating values

Volume of test Pit between 25% and 75% of water depth:

Time Taken to drain between 25% and 75% of water depth:

2

0.43 m3 24.16 min or

**0.403** hr

**Test 2 - Soil Infiltration rate:** 

1.04E-04 m/s 0.37451 m/hr

#### TEST 3

#### **Pit Dimensions:**

L: 1500 mm W: 700 mm D: 1000 mm

Key	_
	Input
	Calculation

Ti	1	
Time Since Start	Water Level from GL	Depth of water
min	mm	mm
0	181	819
10	472	528
20	647	353
30	749	251
40	900	100
50	1000	0

Mean Surface Area
Depth of water
Time at 25% or at

Depth of water

204.8

mm
mm of water
Interpolating Values
Time Water Depth

30
251
40
100

Time at 75% or at 614.3 mm of water Interpolating Values
Time Water Depth
0 819
10 528

7.036 min. From interpolating values

33.06 min. From interpolating values

Volume of test Pit between 25% and 75% of water depth: Time Taken to drain between 25% and 75% of water depth:

0.43 m3 26.03 min or

**0.434** hr

Test 3 - Soil Infiltration rate:

9.65E-05 m/s 0.34758 m/hr

**SOAKAWAY TRIAL PIT 3 INFILTRATION RATE** 

9.65E-05 m/s 0.34758 m/hr

Project:	Land North Of Milton Road, Adderbury	
Calculation By:	Mario Mora	
Title :	Soakaway Calculation	RIVA
Date:	19/10/2022	

# Results

# **SOAKAWAY TRIAL PIT 1 INFILTRATION RATE**

INFILTRATION RATE

**5.12E-05** m/s **0.18450** m/hr

# **SOAKAWAY TRIAL PIT 3 INFILTRATION RATE**

**INFILTRATION RATE** 

9.65E-05 m/s 0.34758 m/hr

MINIMUM INFILTRATION RATE

5.12E-05 0.18450