Flood estimation report: Land at North West Bicester, Oxfordshire.

Introduction

This report template is a supporting document to the Environment Agency's Flood Estimation Guidelines. It provides a record of the hydrological context, the method statement, the calculations and decisions made during flood estimation and the results. This document can be used for one site or multiple sites. If only one site is being assessed, analysts should remove superfluous rows from tables.

Guidance notes (in red text) are included throughout this document in column titles or above tables. These should be deleted before finalising the document. Where relevant, references to specific sections of the Flood Estimation Guidelines document are included to indicate where further useful information can be found.

Note: Column size / page layout can be adapted, where necessary, to best present relevant information, for example, maps do not need to be within the tables if they would be better as a separate page.

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Approval

Note: This table can be amended / removed to suit the need of the organisation undertaking the assessment. A document revision history can be added after the approval table if required.

If a separate method statement stage is not undertaken add N/A to all cells for method statement and also for initial calculations preparation 'Amendments' column. If a separate method statement is generated, text in initial calculations preparation 'Amendments' could be, for example, 'Completion of calculations following method statement approval'. Revision rows are intended for studies where amendments may be required following application of flows to a hydraulic model which leads to estimates / approaches needing to be revisited, for example.

Revision stage	Analyst / Reviewer name & qualifications	Amendments	Date
Method statement preparation	Alejandro Marcotegui	Statistical and ReFH analysis NRFA peak dataset v10	02/05/2023
Method statement sign-off	Simon Mirrams	N/A	15/09/2023
Initial calculations preparation	Alejandro Marcotegui		15/09/2023

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Initial calculations sign-off		N/A	
Calculations - Revision 1 preparation	Alejandro Marcotegui	EA first review comments	01/05/2024
Calculations - Revision 1 sign-off		N/A	
Calculations - Revision 2 preparation			N/A
Calculations - Revision 2 sign-off		N/A	

Abbreviations

AEP	annual exceedance probability
AM	Annual Maximum
AREA	Catchment area (km²)
BFI	Base Flow Index
BFIHOST	Base Flow Index derived using the HOST soil classification
CPRE	Council for the Protection of Rural England
FARL	FEH index of flood attenuation due to reservoirs and lakes
FEH	Flood Estimation Handbook
FSR	Flood Studies Report
HOST	Hydrology of Soil Types
NRFA	National River Flow Archive
OS	Ordnance Survey
POT	Peaks Over a Threshold
QMED	Median Annual Flood (with return period 2 years)
ReFH	Revitalised Flood Hydrograph method
ReFH2	Revitalised Flood Hydrograph 2 method
SAAR	Standard Average Annual Rainfall (mm)
SPR	Standard percentage runoff
SPRHOST	Standard percentage runoff derived using the HOST soil classification
Тр(0)	Time to peak of the instantaneous unit hydrograph
URBAN	Flood Studies Report index of fractional urban extent
URBEXT1990	FEH index of fractional urban extent
URBEXT2000	Revised index of urban extent, measured differently from URBEXT1990
WINFAP-FEH	Windows Frequency Analysis Package – used for FEH statistical method

1 SUMMARY OF ASSESSMENT

1.1 Summary

This table provides a summary of the key information contained within the detailed assessment in the following sections. The aim of the table is to enable quick and easy identification of the type of assessment undertaken. This should assist in identifying an appropriate reviewer and the ability to compare different studies more easily.

The aim of this table is to provide a summary so keep the text to one or two sentences for each point.

Catchment location	
Purpose of study and scope e.g. for scope just include whether it is simple, routine, moderate, difficult, very difficult	The purpose of this study is to assess the peak flows and design strom of the catchment located north west Bicester, the site is crossed by three ordinary watercourses and at its confluence crosses the Lords Lane (A4095) towards Bicester. Therefore, the calculation of adequate flows shojld help to determine the current flood risk at the development site and the possible mitigation options. The catchment complexity is considered as moderate.
Key catchment features e.g. permeable, urban, pumped, mined, reservoired	The catchment is mostly rural currently greenfield.
Flooding mechanisms e.g. fluvial, surface water, groundwater	The main flooding mechanisnt at this catchment is specifically fluvial for the three watercoruses and its confluence
Gauged / ungauged State if there are flow or level gauges and a very brief indication of quality if there are	According to the NRFA , the unnamed watercourse crossing the development site is an ungagged catchment. None of the three rivers has any gauge.
Final choice of method	The ReFH2 hydrographs has been fitted to the statistical analysis peak flows.
Key limitations / uncertainties in results	

1.2 Note on flood frequencies

The frequency of a flood can be quoted in terms of a return period, which is defined as the average time between years with at least one larger flood, or as an annual exceedance probability (AEP), which is the inverse of the return period.

Return periods are are output by the Flood Estimation Handbook (FEH) software and can be expressed more succinctly than AEP. However, AEP can be helpful when presenting results to members of the public who may associate the concept of return period with a regular occurrence rather than an average recurrence interval. <u>Results tables in this document contain both return period and AEP titles; both rows can be retained or the relevant row can be retained and the other removed, depending on the requirement of the study.</u>

The table below is provided to enable quick conversion between return periods and annual exceedance probabilities.

Annual exceedance probability (AEP) and related return period reference table

AEP (%)	50	20	10	5	3.33	2	1.33	1	0.5	0.1
AEP	0.5	0.2	0.1	0.05	0.033	0.02	0.0133	0.01	0.005	0.001
Return period (yrs)	2	5	10	20	30	50	75	100	200	1,000

2 METHOD STATEMENT

For all but simple or routine projects, establish a break-point in which the method statement is reviewed before work continues. This creates a valuable opportunity to agree on the intended approach and address any difficulties with availability of data or information from previous work.

2.1 **Requirements for flood estimates**

 Overview The content and level of detail provided in this section will depend on the scope of the study. The following should be included as a minimum: Purpose of study Peak flows or hydrographs? Design events for which flow estimates are to be made given as AEP (%) Climate change allowances with reference to reference to reference to relevant guidance Potential number of locations for
flow estimation The purpose of the document
Project scope What is the complexity of the study – simple, routine, moderate, difficult, very difficult?
What analyses need to be included within the study, for example: • Review of existing studies? • Conter FSR have been studied in the presentation of this report the Land ad No West Bicester (Firethorn Developments Limited-Vectos 2021).
• Rating reviews / updates? Also the Langford Brook (Bicester) & Pingle-Back-Pure model (2010) was analys for this report.
 Simple / detailed flood history review? ReFH model parameter Additionally a Preliminary Opinion Request was requested in February 2023 order to asses the Model and Flood Study methodology and the request was rejected.
estimation?Joint probability?

2.2 The catchment

Include a map of the catchment in here, at a minimum showing the river network, catchment boundary and gauging stations, and appropriately labelled / referenced in a legend. Additional information which could be included is the model extent or locations of unusual / interesting features, for example. Think about the background mapping being used scale and colour / greyscale - think about if the reader could easily identify locations from the background mapping. Include more than one map if that would assist in presenting the information, consider including maps using satellite imagery as background if that would better show key catchment features, and consider including photographs if they would help understanding of features identified in the 'Description' section. For permeable catchments, consider including a hydrogeological map showing groundwater equipotential lines. Remember to give all figures a number and title and refer to them in the text. In many cases it will be best to present maps outside of this box. Consider changing the page orientation to landscape and the page size to A3 if necessary. The three ordinary watercourse that cross the site are located within the FEH Description Include topography, climate, Catchment 457650, 224000 and drains a total area of 10.53km2.

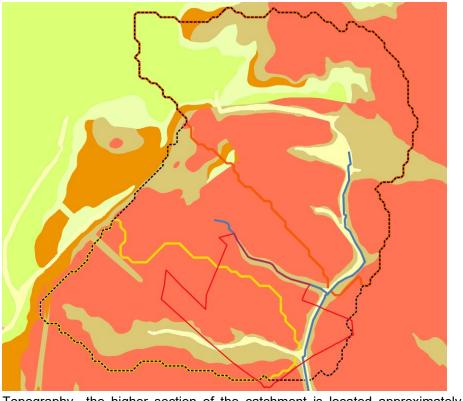
geology, soils, land use and

any unusual features (e.g. reservoirs, historic mining) that may affect the flood hydrology. In some cases, it may be useful to include reference to things such as amount of modelled reach that is culverted but remember that this is not a hydraulic modelling report and detail on hydraulic features, such as weir and culvert sizes, is not required. Think about what features are going to affect runoff from the contributing catchment reaching the watercourse.

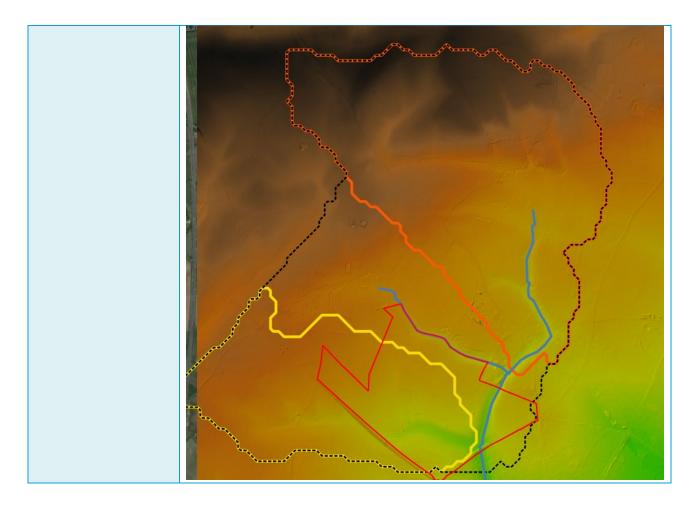


The catchment is mostly rural with a URBEXT of 0.0077 for the entire catchment (0.13km2)

The gelogy of the catchment it is almost entirely Cornbrash Formation (Limestone)-(pale red) with superficial geology of Alluvium depositns (sand, silt, and gravel) at the river margins (yellow). And Forest Marbe Formation. (brown) Parts fo the upper catchmnt section are White Limestone formation.



Topography the higher section of the catchment is located approximately at 115mAOD at the north west and the lower section approximately at 79mAOD after the crossing of the A4095 road.



2.3 Source of flood peak data

This should be updated to the latest version of the dataset at the time of the assessment.

Source	NRFA peak flows dataset, Version 11.1.1, released in March 2023. Winfap version 5.0.8181

2.4 Gauging stations (flow or level)

Only need to include gauges at or very near to the sites of flood estimates unless there is an exceptional reason to include other gauges.

Note: If you have data extracted from WISKI the datafile may only provide the digital data period of record, and the actual operating period of the gauge may be longer. It is useful to check this.

Water- course	Station name	Gauging authority number	NRFA number	Catchment area (km²)	Type (rated / ultrasonic / level)	Start of record and end if station closed
n/a						

2.5 Data available at each flow gauging station in Table 2.4

This table can be deleted if the study catchment is ungauged.

A quality check of the data is not required if the gauge is in the NRFA, unless specifically called for in the project brief.

There is no need to repeat everything in the NRFA station description, for example, weir length, wingwall height. Just add the key factors which will affect the quality of flood flow measurement and hence confidence

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in the data. For more detailed studies consider looking for other sources of information, for example, gauging authority rating review reports, station files held at CEH Wallingford, or reports on earlier flood studies.

Station name	Start and end of NRFA flood peak record	Update for this study?	OK for QMED?	OK for pooling ?	Data quality check needed?	Other comments on station and flow data quality
n/a						
Tabulate any u provide a link h	pdated or revised ere.	l flood peak se				
	data not in the N hould be provide					
Give link/refere Delete this row	nce to any furthe if not relevant.	er data quality c				

2.6 Rating equations

This table can be deleted if the catchment is ungauged or if all gauges are in the NRFA and a rating review is not requested in the project brief.

-More information on rating reviews is provided in Section 2.1 of the Flood Estimation Guidelines.

Station name	Type of rating e.g. theoretical, empirical; degree of extrapolation	Rating review needed?	Comments and link to any rating reviews
n/a			

2.7 Other data available and how it has been obtained

Type of data	Data relevant to this study?	Data available?	Source of data	Details
Check flow gaugings (if planned to review ratings)				
Historical flood data Include chronology and interpretation of flood history in Annex or separate report. The detail included will depend on requirements in the project scope. If there is a flow gauge within the study reach (or close by), consider if the historical flood data could be used to extend the systematic gauge record (see FEH Local guidance for more information)	Two different FSR a vectos 2021 and EA 2010 has been review			Vectos study represents only a section of the entire catchment, however some of the assumptions has been analysed and expored. EA model upstream section represents the downstream section of this model therefore some the flow can be compared and adjusted accordingly.
Flow or river level data for events				
Rainfall data for events				
Potential evaporation data This may be required if the ReFH2 Calibration Utility is being used	n/a data not found			

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Results from previous studies	Vectos and EA	The data has been analysed and adjusted accordingly
Other data or information (e.g. groundwater, tides, channel widths, low flow statistics, sewer network data)	n/a	

2.8 Hydrological understanding of catchment

This table can be deleted if the catchment is ungauged. The second table (conceptual model and unusual features) should not be deleted as this information is relevant for all catchments / studies.

The table below is an opportunity to assess any catchment river gauge data to provide an understanding of the hydrological behaviour of a watercourse. Examples of information which could be here are:

- Plots of flow data, for example, annual flow hydrographs or example flood events. This should be followed by an interpretation of the plots, for example, discussion of catchment processes, response time, propagation of a flood, and contributions from tributaries. If there is more than one gauge in the study area it can be useful to plot the data for all gauges on the same graph as this can aid understanding of the relationship between flow at different locations. These plots can be useful for checking the quality of the data and it is often helpful to plot flow and rainfall together as this may identify problems.
- Plots of stage data. Many catchments do not have flow gauges, but stage / level data may be available. This data can provide valuable information on the catchment response in the absence of flow data.
- Plots of flood peak data. This could be the AMAX series or the POT series. Visually examine the time series and identify if there are, for example, outliers, apparent truncation of the flood peaks, trends or fluctuations in the data, step changes in the data, or unusually small flows. An interpretation of these and other features should be provided. If there is more than one gauge in the study area, correlation plots can help to identify patterns or inconsistencies in the hydrological behaviour. Also consider adding other informative plots, for example, showing the seasonality of floods or the correlation of peak flows at different gauges.

More information is provided in Section 2 of the Flood Estimation Guidelines.

Add rows to the table if required and change titles in the left column if necessary.

Plots of flow data and interpretation	
Plots of flood peak data and interpretation	

 Conceptual model Include information on factors such as: Where are the main sites of interest? What is likely to cause flooding at those locations? (peak flows, flood volumes, combinations of peaks, groundwater, snowmelt, tides) Might those locations flood from runoff generated on part of the catchment only, e.g. downstream of a reservoir? Is there a need to consider temporary debris dams that could collapse? 	The proposed development sites lies at the northwest of Bicester, after crossing the A4095 road, the three watercoruses flowing within the development, therefore the understanding of the fluvial flood characteristing and possible risk zones and flow constraints and junction it is paramount to reduce the flood risk anywhere else (third party land including Bicester) so the junction of each tributary is site of interest.
 Unusual catchment features Include information on factors such as: highly permeable heavily urbanised pumped watercourse major reservoir influence (FARL<0.90) flood storage areas, particularly those which are normally dry historical mining or operational mining activities Guidance on methods for unusual catchments is contained in Section 7 of the Flood Estimation Guidelines 	The catchment is not highly permeable and as is set previously is considered mostly rural, also there are not any reservoirs or flood strage areas within the are of study nor upstream section.

2.9 Initial choice of approach

Is FEH appropriate? (it ma	ay not be for extremely	Yes the FEH method is appropriate, as	the catchmetn is
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heavily urbanised or complex catchments). If not, describe other methods to be used.	mostly rural. Therefore the use of statistical data fitted to the ReFH2 hydrographs provide reliable results.
Initial choice of method(s) and reasons Think about: (i) the type of problem, (ii) the type of catchment, and (ii) the type of data available. Which methods are appropriate? If more than one method is appropriate will all be applied, and the results compared	Statistical analysis Hydrograph and design storm provided by ReFH2 The catchmetn ahs been analysed against topographical
before a final decision is made? How will hydrograph shapes be derived if needed?	contours and created the sub-catchments according to each drainage location.
e.g. ReFH1 / ReFH2 shapes, average hydrograph shape from gauge data Will the catchment be split into sub- catchments? If so, how?	The design storm duration was analysed with ReFH hydrograph and it is considered that 13h storm produce reliable results.
If the hydrological assessment is being undertaken to supply inflows to a hydraulic model, it is likely that a distributed approach will be taken, with the catchment split into sub-catchments and design flows routed from each sub-catchment. Think about what the split into	Various FEP has been obtained from the different sub- cathcments.
sub-catchments will be based on, e.g. tributary confluences, changes in geology / urbanisation, key areas of interest, sewer outfalls. Will intervening area hydrographs be required and how will these be derived? If the catchment area changes significantly over the study reach, or tributaries are also being modelled, will different storm durations need to be considered / tested?	FEH analysis is included within thispackage files at the <i>Model</i> \1D_FMP\FEH files, for each subacthment.
Software to be used (with version numbers) Delete entries in the column on the right as appropriate	FEH Web Service ¹ / WINFAP 5 ² / ReFH spreadsheet / ReFH2.2 / Flood Modeller Pro 7.0

² WINFAP 4 © Wallingford HydroSolutions Limited 2016.

¹ CEH 2015. The Flood Estimation Handbook (FEH) Online Service, Centre for Ecology & Hydrology, Wallingford, UK.

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3 LOCATIONS WHERE FLOOD ESTIMATES REQUIRED

Consider including a map here which shows the locations of flood estimate locations.

The table below lists the locations of subject sites. The site codes listed below are used in all subsequent tables to save space.

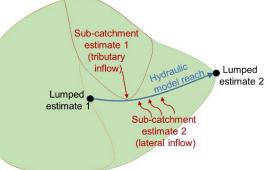
Include any intervening areas required for a distributed approach in here as these are necessary to reproduce results.

Site code	Type of estimate L: lumped catchment S: Sub- catchment	Watercourse	Name or description of site	Easting	Northing	AREA on FEH CD- ROM (km ²)	Revised AREA if altered
East	L	No name	Watercourse draining south collecting all other tributaries (upper section)	457900	224950	5.26	5.26
West	L	No name	Watercourse flowing east confluence before the crossing with A4095	57550	24250	2.79	2.79
North	L	No name	Flowing east confluence at the north section of the	57800	24950	1.89	1.89
Downstre am	L	No name	All the subcatchments	457650	224000	10.53	10.53

Note: Lumped catchments (L) are complete catchments draining to points at which design flows are required.

Sub-catchments (S) are catchments or intervening areas that are being used as inputs to a semi-distributed model of the river system. There is no need to report any design flows for sub-catchments, as they are not relevant: the relevant result is the hydrograph that the sub-catchment is expected to contribute to a design flood event at a point further downstream in the river system. This will be recorded within the hydraulic model output files. However, catchment descriptors and ReFH model parameters should be recorded for sub-catchments so that the results can be reproduced.

The schematic diagram illustrates the distinction between lumped and sub-catchment estimates.



3.2 Important catchment descriptors at each subject site (incorporating any changes made)

Consider using a different colour text / highlighting to identify catchment descriptors which have been changed from the FEH values.

Include any intervening areas required for a distributed approach in here as these are necessary to reproduce results.

Site code	FARL	PROPWET	BFIHOST DPLBAR (km)		DPSBAR (m/km)	SAAR (mm)	URBEXT 1990 Delete if not required	URBEXT 2000	FPEXT	
East	0.949	0.32	0.770	2.64	17.5	654		0.0062	0.0855	
West			0.32	0.845	1.72	14.2	639		0.0040	0.0915
North			0.799	1.63	18.4	647		0.0241	0.0614	
DS	0.974	0.32	0.857	2.94	16.7	647		0.0077	0.087	

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Site code	FARL	PROPWET	BFIHOST	DPLBAR (km)	DPSBAR (m/km)	SAAR (mm)	URBEXT 1990 Delete if not required	URBEXT 2000	FPEXT

3.3 Checking catchment descriptors

Record how catchment boundary was checked and describe any changes Add maps if needed to aid explanation of any changes If changes are made to the catchment boundary (and hence AREA), identify if any other descriptors will be updated and how	Catchmet boundaries have been checked against contours and none of then have been amended.						
Record how other catchment descriptors were checked and describe any changes. Include before/after table if necessary.	No changes						
Source of URBEXT Delete as needed. URBEXT1990 is only used for ReFH1 An alternative is the URBAN50k method if URBEXT values need to be substantially revised due to discrepancies between the FEH urban extent layers and current mapping	URBEXT2000 no changes Box 6.1 Categories of catchment urbanisation Six categories of catchment urbanisation are distinguished in the FEH, according to their URBEXT values. Essentially rural 0.000 ≤ URBEXT < 0.025 Slightly urbanised 0.025 ≤ URBEXT < 0.050 Moderately urbanised 0.125 ≤ URBEXT < 0.125 Heavily urbanised 0.125 ≤ URBEXT < 0.250 Very heavily urbanised 0.250 ≤ URBEXT < 0.500 Extremely heavily urbanised 0.500 ≤ URBEXT ≤ 1.000						
Method for updating of URBEXT Delete as needed (CPRE formula from FEH Volume 4 is for URBEXT1990) An update to the current year is not required when the URBAN50k method is used as it will be implicitly accounted for in the latest mapping	CPRE formula from FEH Volume 4 / CPRE formula from 2006 CEH report on URBEXT2000 n/a						

4 STATISTICAL METHOD

4.1 Application of Statistical method

What is the purpose of	All catchmetn analysed in this report are greater that 50ha, additionally the
applying this method?	statistical analysis with provide better approach as will use pooling station of
Brief summary of the reasons,	catchmetn with similatities as the studied in this report, therefore is expected
specific to this study, for applying	to bring reliable results.
the method. For example, lumped estimates at key locations	Additionally the requirements of peak flows at the selected FEP can bring
for the purpose of checking	estimated parameters fo this study.
modelled peak flow estimates.	

4.2 Overview of estimation of QMED at each subject site

If more than one donor is used, use multiple rows for the site and give the weights used in the averaging. Record the weighted average adjustment factor in the penultimate column.

The final estimate of QMED should include any relevant donor and urban adjustment. If QMED is derived directly from AMAX or POT data, an urban adjustment factor should not be applied as this is implicitly included in the estimate and would be double-counted.

				Data	transfer						
		NRFA numbers for donor		Moderat QMEI adjustm)		re than donor	Urban	Final		
Site code	(rural) from CDs (m³/s)	Final method	sites used (see 4.3)			, a	Weight	Weighted ave. adjustment	adjust- ment factor UAF	estimate of QMED (m³/s)	
DS	0.429	CD	39002	29					1.020	0.444	
East											
North											
West											
Are the va	lues of QM	ED sp	atially consis	tent?							
			stment for su				Kjeldsen (2010) ³ / WINFAP v4 ⁴				
	rs used for values have b			n adjustment	if applica	able (t	hese ar	e 'standar	d' values and sho	ould be revised	
Impervious up areas,	s fraction fo IF	or built		age runoff for ous surfaces,			hod fo er, UR		lating fracti	onal urban	
0.3			70%	70%			From updated URBEXT2000				
0.3 70% From updated URBEXT2000 Notes Methods: AM – Annual maxima; POT – Peaks over threshold; DT – Data transfer (with urban adjustment); CD – Catchment descriptors alone (with urban adjustment); BCW – Catchment descriptors and bankfull channel width (add details); LF – Low flow statistics (add details). The QMED adjustment factor A/B for each donor site is moderated using the power term, a, which is a function of the distance between the centroids of the subject catchment and the donor catchment. The final estimate of QMED is (A/B) ^a times the initial (rural) estimate from catchment descriptors. Important note on urban adjustment The method used to adjust QMED for urbanisation published in Kjeldsen (2010) ³ in which PRUAF is calculated from BFIHOST is not correctly applied in WINFAP-FEH v3.0.003. Significant differences occur only on urban catchments that are highly permeable. This is discussed in Wallingford HydroSolutions (2016) ⁴ .											

 ³ Kjeldsen, T. R. (2010). Modelling the impact of urbanization on flood frequency relationships in the UK. Hydrol. Res. 41. 391-405.
 ⁴ Wallingford HydroSolutions (2016). WINFAP 4 Urban adjustment procedures.

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Comment on potential donor sites
Provide details regarding how potential donors were selected and the reasons why they were chosen / rejected.
Include a map if necessary, which shows the location of the study catchment and donor stations under consideration.
Section 4 of the Flood Estimation Guidelines provides guidance on selecting a donor(s) for data transfer.

4.4 Donor sites chosen and QMED adjustment factors

When QMED is estimated from POT data, it should also be adjusted for climatic variation; this is not the same as climate change. Climatic variability can result in flood-rich or flood-poor periods. A short record might only include flood-rich years or flood-poor years, this will distort the QMED estimate. FEH Volume 3, Chapter 20, provides the methodology to adjust QMED for climatic variation. It is recommended that this carried out if the station record is shorter than 14 years.

QMED from catchment descriptors is the 'as rural' value (for rural donors), i.e. with no urban adjustment factor applied.

NRFA no.	Method (AM or POT)	Adjustment for climatic variation?	QMED from flow data (A)	QMED from catchment descriptors (B)	Adjustment ratio (A/B)
39002	AM	NO			

The adjustment ratio is the adjustment in full, with no distance factor applied.

4.5 Derivation of pooling groups

Try to use as few groups as possible, this avoids step changes in flow estimates between flow estimation points for catchment-wide studies. If all catchments being assessed have AREA <25km² and similar SAAR, FARL and FPEXT values, normally use one group.

Section 4.3 of the Flood Estimation Guidelines provides further details on reviewing pooling groups.

Name of group	Site code from whose descriptors group was derived	Subject site treated as gauged? (enhanced single site analysis)	Changes made to default pooling group, with reasons (if there are no changes just say "None", although it is helpful to provide details of stations which were investigated even if they were ultimately retained)	Weighted average L- moments L-CV and L-skew, (before urban adjustment)
DS	7011	no	Low data ~9yr	0.491-0.521
DS	26013		Low data @11yr	0.281-0.196

Note: Pooling groups were derived using the procedures from Science Report SC050050 (2008).

4.6 Derivation of flood growth curves at subject sites

Any relevant frequency plots from WINFAP, particularly showing any comparisons between single-site, enhanced single-site and pooled growth curves (including flood peak data on the plot), should be shown here.

An individual urban adjustment should be applied even if the same pooling group (including enhanced singlesite analysis) has been applied to several sites, as each site is likely to have a different URBEXT2000 value and hence a different urban adjustment.

For single-site analysis on a permeable catchment, or a pooled analysis for a group consisting largely of permeable catchments, a permeable adjustment should be applied to the growth curve using the technique described in the FEH Volume 3, Chapter 19 for removing flood-free years by adjusting the L-moments.

Site code	Method (SS, P, ESS, J)	If P, ESS or J, name of pooling group	Distribution used and reason for choice	Note any urban adjustment or permeable adjustment	Parameters of distribution (location, scale and shape after adjustments)	Growth factor for 100-year return period / 1% AEP (delete as needed)
27073	Р	DS only	GL	-		DS- RURAL 3.060
26016	Р		GL	-		DS URBAN 3.056
25019	Р		GL	-		
36010	Р		GL	-		
27051	Р		GL	-		
26014	Р		GL	-		
39033	Р		GL	-		
33054	Р		GL	-		
36004	Р		GL	-		
24007	Р		GL	-		
27010	Р		GL	-		
41020	Р		GL	-		
33032	Р		GL	-		
53017	Р		GL	-		
9006	Р		GL	-		

Methods: SS – Single site; P – Pooled; ESS – Enhanced single site; J – Joint analysis

Urban adjustments are all carried out using the method of Kjeldsen (2010).

Growth curves were derived using the procedures from Science Report SC050050 (2008).

4.7 Flood estimates from the statistical method

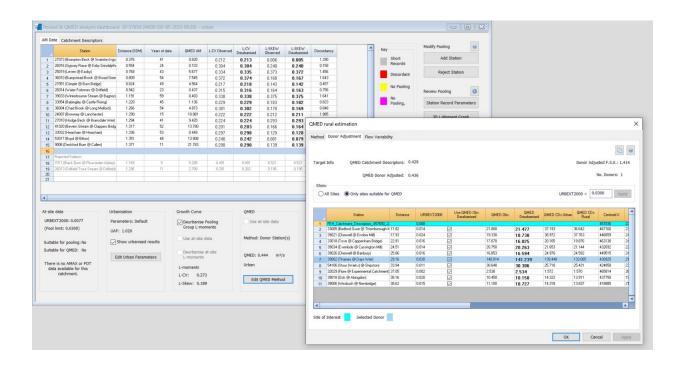
Site code		Flood	peak (m	n³/s) for t	the follo	wing ret	turn peri	iods (in y	years)			
	2	5	10	20	25	30	50	100	500	1000		
	Flood peak (m ³ /s) for the following AEP (%) events											
DS urban	0.444	0.642	0.784	0.936	0.988	1.03	1.16	1.36	1.92	2.22		
East								0.754		1.667		
North								0.414		0.799		
West								0.244		0.541		

	\$				Suitability	Export Site		Single Site analysis
Number	3858976468		Grid reference	457650, 224000	Pooling	Exportaile		Station Fittin
Name	FEH_Catchment_Descrip	tors	Catchment area (km²)	10.53	OMED	Edit details	-	Individual Distribu
Location	SP 57650 24000					Eult details		Time Series Gr
							^	Flood Frequency
								Select Distribu
								Standardis 🗸
								>
atchment De	scriptors							
IHDTM NGR	GB, 457650, 224000	Edit	LDP	6.12	Edit			
	R GB, 457036, 225869	Edit	PROPWET	0.32	Edit			
DTM AREA	10.5325	Edit	RMED-1D	31.4	Edit			
ALTBAR	99	Edit	RMED-1H	10.2	Edit			
ASPBAR	146	Edit	RMED-2D	38.8	Edit			
ASPVAR	0.58	Edit	SAAR	647	Edit			
BFIHOST	0.857	Edit	SAAR4170	662	Edit			
BFIHOST19	0.802	Edit	SPRHOST	13.07	Edit			
DPLBAR	2.94	Edit	URBCONC1990	-1.000	Edit			
DPSBAR	16.7	Edit	URBEXT1990	0.0018	Edit			
FARL	0.974	Edit	URBLOC1990	nan	Edit			
FPEXT	0.0873	Edit	URBCONC2000	0.574	Edit			
FPDBAR	0.4900	Edit	URBEXT2000	0.0077	Edit			
	0.8660	Edit	URBLOC2000	1.116	Edit			

MED				
Using catchment descriptors	QMED _{cds} Rural	0.429	mº/s	
	QMED _{cds} Urban	0.438	m ^o /s	

	Station	Distance (SDM)	Years of data	QMED AM	L-CV Observed	L-CV Deurbanised	L-SKEW Observed	L-SKEW Deutbanised	Discordancy	-	Кеу	Modify Pooling	9		
1	27073 (Brompton Beck @ Snainton Ings	0.376	41	0.820	0.212	0.213	0.006	0.005	1.074		Short	Add St	ation		
2	26016 (Gypsey Race @ Kirby Grindalythe	0.554	24	0.103	0.304	0.304	0.240	0.240	0.103		Records				
3	25019 (Leven @ Easby)	0.768	43	5.677	0.334	0.335	0.373	0.372	0.716		Discordant	Reject S	tation		
4	36010 (Bumpstead Brook @ Broad Gree	0.809	54	7.545	0.372	0.374	0.168	0.167	1.448		Discordant				
5	27051 (Crimple @ Burn Bridge)	0.824	49	4.564	0.217	0.218	0.143	0.142	0.392		No Pooling				
6	26014 (Water Forlomes @ Driffield)	0.942	23	0.437	0.315	0.316	0.164	0.163	0.319		No Fooling	Review Pooling	0		
7	7011 (Black Burn @ Pluscarden Abbey)	1.169	9	5.205	0.491	0.491	0.521	0.521	2.688		No				
8	39033 (Winterbourne Stream @ Bagnor)	1.191	59	0.403	0.338	0.338	0.375	0.375	1.233		Pooling,	Station Record	Parameters		
9	33054 (Babingley @ Castle Rising)	1.220	45	1.136	0.229	0.229	0.183	0.182	0.664		-				
10	36004 (Chad Brook @ Long Melford)	1.266	54	4.873	0.301	0.302	0.170	0.169	0.808			3D L-Mome	ant Granh		
11	24007 (Browney @ Lanchester)	1.290	15	10.981	0.222	0.222	0.212	0.211	1.368		Total years: 662	50 L-Morrie	incoroph		
12	27010 (Hodge Beck @ Bransdale Weir)	1.294	41	9.420	0.224	0.224	0.293	0.293	1.356		1 0101 YEDI 5. 002	- Discourse and the second sec			
13	26013 (Driffield Trout Stream @ Driffield)	1.296	11	2.700	0.281	0.282	0.196	0.195	2.348		Heterogeneity			- 0	
14	41020 (Bevern Stream @ Clappers Bridg	1.317	52	13.780	0.201	0.203	0.166	0.164	0.883		Theterogeneny	THE BUILDING	100		
15	33032 (Heacham @ Heacham)	1.336	53	0.449	0.297	0.298	0.129	0.128	0.364		Number of sim	ulations 500	Apply		
16	53017 (Boyd @ Bitton)	1.351	48	13.908	0.240	0.242	0.081	0.079	0.457						
17	9006 (Deskford Burn @ Cullen)	1.371	11	21.783	0.290	0.290	0.139	0.139	0.375						
18	44008 (South Winterbourne @ Winterbo	1.381	30	0.496	0.421	0.422	0.289	0.289	1.404						
19											L-CV/L-skew	ness distance			
20											Observed av	/oracio	0.1092		
21 22					-							2	0.0781		
22										-		ean of average	0.0124		
-										1.22	Simulated S.	D. of average			
•										•	Standardise	d test value H2	2.5146		
t-site	data Urba	anisation	(Frowth Curve		QMED		R	Results			group is heteroge	neous and a r	eview of	
upper	XT2000: 0.0077 Par			_							the pooling	group is desirable.			
	limit: 0.0200)	ameters: Defaul	t l	Deurbanise F Group L-mor		Use a	t-site data		Report						
	UAI	F: 1.020		Use at-site d	ata	Method:	Donor Station	(s)	Select Distributions		Standard devi	ation of L-CV			
Suita	ble for pooling: No	Show urbanised	results	obe or one o	ure .						Observed		0.0666		
Suita	ble for QMED: No			Development					Growth Curve		Simulated m		0.0345		
	Contraction Contraction Contraction	dit Urban Param	neters	Deurbanise a L-moments	at-site	QMED: 0	.353 m³/s	i i	Fittings Graph						
1210	e is no AMAX or POT	and an out it all dif		e-mornelius					a ange arapin		Simulated S.	D.	0.0061		
	a available for this			L-moments		Rural			Flood Frequency Curve		Standardise	d test ∨alue H1	5.2342		
	catchment.			L-CV: 0.291					Fittings Graph		Strongly He				

<u>1.1</u>



M Da	ta Catchment Descriptors Station	Distance (SDM)	Years of data	QMED AM	L-CV Observed	L-CV Deurbanised	L-SKEW Observed	L-SKEW Deurbanised	Discordancy		Кеу	Modify Pooling	۲
1	27073 (Brompton Beck @ Snainton Ings	0.376	41	0.820	0.212	0.213	0.006	0.005	1.290		Short	Add Station	
2	26016 (Gypsey Race @ Kirby Grindalyth		24	0.103	0.304	0.304	0.240	0.240	0.158		Records		
3	25019 (Leven @ Easby)	0.768	43	5.677	0.334	0.335	0.373	0.372	1.456		-	Reject Station	
4	36010 (Bumpstead Brook @ Broad Gree	0.809	54	7.545	0.372	0.374	0.168	0.167	1.643		Discordant		
5	27051 (Crimple @ Burn Bridge)	0.824	49	4.564	0.217	0.218	0.143	0.142	0.457				
6	26014 (Water Forlornes @ Driffield)	0.942	23	0.437	0.315	0.316	0.164	0.163	0.756		No Pooling	Review Pooling	0
7	39033 (Winterbourne Stream @ Bagnor)	1.191	59	0.403	0.338	0.338	0.375	0.375	1.641		No	Review Fooling	•
8	33054 (Babingley @ Castle Rising)	1.220	45	1.136	0.229	0.229		0.010			bling	Station Record Param	neters
9	36004 (Chad Brook @ Long Melford)	1.266	54	4.873	0.301	0.302	Heterog	eneity measu	ires		X		
10	24007 (Browney @ Lanchester)	1.290	15	10.981	0.222	0.222	-						
11	27010 (Hodge Beck @ Bransdale Weir)	1.294	41	9.420	0.224	0.224	Number	of simulations	500	Apply D		3D L-Moment Grag	pn
12	41020 (Bevern Stream @ Clappers Bridg	1.317	52	13.780	0.201	0.203				4	rs: 612	E.	
13	33032 (Heacham @ Heacham)	1.336	53	0.449	0.297	0.298						Catchment Descriptor	Graphs
14	53017 (Boyd @ Bitton)	1.351	48	13.908	0.240	0.242							
15	9006 (Deskford Burn @ Cullen)	1.371	11	21.783	0.290	0.290	L-CV/L-	-skewness dis	tance		-10	All Analysis Graph	hs
16						1	Obser	ved average	0.10	21			
17	Rejected Stations						Simula	ated mean of a	Verage 0.07	79			
18	7011 (Black Burn @ Pluscarden Abbey)	1.169	9	5.205	0.491	0.491			verage			Exploratory data analys	sis
19	26013 (Driffield Trout Stream @ Driffield)	1.296	11	2.700	0.281	0.282		ated S.D. of av	elage			angioratory data analys	
20							Standa	ardised test va	lue H2 1.76	82		Goodness of Fit	
21									s possibly heter I group is option	ogeneous and a al.		Heterogeneity	
						OMED	Standar	d deviation of	L-CV				
t-siti	e data Urb	anisation		Growth Curve		QMED	Obser	hav	0.05	62			
URB	EXT2000: 0.0077 Pa	rameters: Defau	lt	Deurbanise	Pooling	Us							
(Poo	l limit: 0.0300)	F. 1 070		Group L-mo				ated mean	0.03				
	AU	F: 1.020					Simula	ated S.D.	0.00	66			
		Show urbanised	i results	Use at-site data Metho Standardised test value H1 3.4575		ults Standardised test value							
Suita	ble for QMED: No			Deurbanise	at-site	01150	Heter	ogeneous					
		Edit Urban Paran	neters	L-moments		QMED							
	e is no AMAX or POT			L-moments		Rural							
da	ta available for this catchment.								Save	Cancel			
				L-CV: 0.27	4				oave	Cancer			

5 REVITALISED FLOOD HYDROGRAPH (REFH) METHOD

5.1 **Application of ReFH method**

What is the purpose of applying this method?
Brief summary of the reasons, specific to this study, for applying the method. For example,
lumped estimates at key locations for the purpose of checking modelled peak flow estimates,
distributed approach to apply inflows to a hydraulic model, deriving hydrograph shapes only,
extending the flood frequency curve out to extreme events (long return periods).

5.2 Catchment sub-divisions for urban ReFH model

This section can be deleted if the catchment is essentially rural.

If the catchment is urban...

Did you calculate paved areas using a method other than from URBEXT using the standard equations?

Did you allow for transfer of water via sewers across the topographic catchment boundary?

If yes to either of these questions provide details which give sufficient information to understand the process applied and any assumptions made. It may be useful to include a map of sub-catchments here, if not provided earlier in the report.

5.3 Parameters for ReFH model (rural catchments)

Lumped and sub-catchment / intervening areas should be included in this table.

Site code	Method	Tp (hours) Time to peak	C _{max} (mm) Maximum storage capacity	BL (hours) Baseflow lag	BR Baseflow recharge			
East	ReFH2	4.93	906.57	56.43	2.08			
North	ReFH2	3.68	1013.7	52.43	2.21			
West	ReFH2	4.12	1314.39	56.77	2.51			
DS	ReFH2	5.32	906.57	57.77	3.138			
	scription of any flood event carried out (further details should be e annex)	All catchment ahas been adjusted to the same design storm.						
Methods:	OPT: Optimisation, BR: Baseflow recession	fitting, CD: Catchm	ent descriptors, DT:	Data transfer (give	details)			

5.4 Parameters for ReFH model (urban or mixed urban & rural catchments)

Lumped and sub-catchment / intervening areas should be included in this table.

If applying the method in Flood Modeller Pro, Tpurban values are not directly specified by the user; the model works them out from the supplied URBEXT, DPLBAR, etc. It is simpler just to report Tp rather than separate URBEXT, etc, values for rural and urban portions.

Note: ReFH is also implemented in InfoWorks ICM which does not include the urban component.

Site code	Method	Tp _{rural} (hours)	Tp _{urban} (hours)	C _{max} (mm)	PR _{imp} % runoff for impermeable surfaces	BL (hours)	BR

5.5 Design events for ReFH method: Lumped catchments

This table can be deleted if ReFH is not being applied for lumped catchments. Note: ReFH may be applied for both lumped catchments and sub-catchments in a study; if this is the case both this table and the next should be completed.

Storm durations detailed here should be the values for the individual catchments. Lumped flows should be generated using the storm duration relevant to each lumped catchment for comparison with Statistical estimates.

Site code	Urban or rural	Season of design event (summer or winter)	Storm duration (hours)
DS	urban	winter	13hr

5.6 Design events for ReFH method: Sub-catchments and intervening areas

This table can be deleted if ReFH is not being applied for sub-catchments.

This table is included to identify the storm which will be applied to all inflows to a distributed model (see Section 6.1 of the Flood Estimation Guidelines) and avoid the scenario of using a different storm for each inflow to the model.

If there are multiple flood risk areas throughout the model it may be necessary to allow for different storms in different parts of the model by carrying out multiple model runs. Each model run should use the same storm applied to all inflows. Use one row for each storm to be applied. If only one storm is to be applied, delete the additional rows.

If storm duration testing using the hydraulic model is being undertaken ensure that the results are included in the last row of this table when the testing is complete, for example, which duration(s) has been selected and why, what the process will be in terms of presenting model results if more than one duration is selected.

Site code	Season of design event	Storm duration (hours)	Storm area for ARF (if not catchment area)	Reason for selecting storm
All	winter	13	0.966	Maximum peak flow
All				
All				
testing. This row can	be deleted if storm			
duration test undertaken.	ting is not being			

5.7 Flood estimates from the ReFH method: lumped catchments

Note: This table is for recording results for lumped catchments. There is no need to record peak flows from sub-catchments or intervening areas that are being used as inputs to a semi-distributed model of the river system.

Site code	Flood peak (m ³ /s) for the following return periods (in years)									
	Flood peak (m ³ /s) for the following AEP (%) events									

6 REVITALISED FLOOD HYDROGRAPH 2 (REFH2) METHOD

6.1 Application of ReFH2 method

What is the purpose of applying this method?
Brief summary of the reasons, specific to this study, for applying the method. For example, lumped estimates at key locations for the purpose of checking modelled peak flow estimates, distributed approach to apply inflows to a hydraulic model, deriving hydrograph shapes only, extending the flood frequency curve out to extreme events (long return periods).

The ReFH method is usually provided good approach for small catchments, when the cathcmetn is more complex and bigger the use of statistical analysis ofr the different subcatchments is preferrable due to the use of large datasets of hydrometric stations that drain catchments with similar characteristics aas the studied in this project. Therefore, the statistical provide robust results for this analysis.However, the ReFH2 will provide suitable design storm and hydrograph for the hydraulic modelling. For the purpose of this study the downstream FEP is used and Area Reduction Factor ARF for te flows has been selected.

6.2 Catchment sub-divisions for ReFH2 model

This section can be deleted if the catchment is essentially rural.

If the catchment is urban...

Did you calculate paved areas using a method other than from URBEXT using the standard equations?

Did you allow for transfer of water via sewers across the topographic catchment boundary?

If yes to either of these questions provide details which give sufficient information to understand the process applied and any assumptions made. It may be useful to include a map of sub-catchments here, if not provided earlier in the report.

6.3 Parameters for ReFH2 model

Lumped and sub-catchment / intervening areas should be included in this table.

Note: The lower limit of Tp_{rural} is 1.0hr; Tp_{urban} can drop below this.

Note: ReFH2 is also implemented in InfoWorks ICM which does not include the urban component.

Site code	Method	Tp _{rural} (hours)	Tp _{urban} (hours)	C _{max} (mm)	PR _{imp} % runoff for impermeable surfaces	BL (hours)	BR
East	ReFH2			906.57		56.43	2.08
North	ReFH2			1013.7		52.43	2.21
West	ReFH2			1314.39		56.77	2.51
DS	ReFH2	5.322	3.99	906.57		57.77	3.138
analysis carri be g	otion of any flo ed out (further d iven in the annex)	etails should					

Methods: OPT: Optimisation, BR: Baseflow recession fitting, CD: Catchment descriptors, DT: Data transfer (give details)

6.4 Design events for ReFH2 method: Lumped catchments

This table can be deleted if ReFH2 is not being applied for lumped catchments. Note: ReFH2 may be applied for both lumped catchments and sub-catchments in a study; if this is the case both this table and the next should be completed.

Storm durations detailed here should be the values for the individual catchments. Lumped flows should be generated using the storm duration relevant to each lumped catchment for comparison with Statistical estimates.

Site code	Urban or rural	Season of design event (summer or winter)	Storm duration (hours)
DS	urban	winter	13
East	urban	winter	
North	urban	winter	
West	urban	winter	

6.5 Design events for ReFH2 method: Sub-catchments and intervening areas

This table can be deleted if ReFH2 is not being applied for sub-catchments.

This table is included to identify the storm which will be applied to all inflows to a distributed model (see Section 6.1 of the Flood Estimation Guidelines) and avoid the scenario of using a different storm for each inflow to the model.

If there are multiple flood risk areas throughout the model it may be necessary to allow for different storms in different parts of the model by carrying out multiple model runs. Each model run should use the same storm applied to all inflows. Use one row for each storm to be applied. If only one storm is to be applied, delete the additional rows.

If storm duration testing using the hydraulic model is being undertaken ensure that the results are included in the last row of this table when the testing is complete, for example, which duration(s) has been selected and why, what the process will be in terms of presenting model results if more than one duration is selected.

Site code	Season of design event	Storm duration (hours)	Storm area for ARF (if not catchment area)	Reason for selecting storm
All	winter	13	0.966	Major peak flow
All				
All				
testing. This row can	storm duration be deleted if storm ting is not being		t bring maximum pea e Statistical analysis.	ak flow, however the peak will be

6.6 Flood estimates from the ReFH2 method

Note: This table is for recording results for lumped catchments. There is no need to record peak flows from sub-catchments or intervening areas that are being used as inputs to a semi-distributed model of the river system.

Site code	Flood peak (m ³ /s) for the following return periods (in years)									
	2	5	10	30	50	100	200	1000		
		Flo	od pea	k (m³/s)	for the	followir	ng AEP	(%) eve	nts	
East	0.286	0.399	0.483	0.631	0.712	0.839	0.992	1.484		
North	0.105	0.148	0.181	0.238	0.269	0.317	0.375	0.532		
West	0.090	0.129	0.158	0.210	0.239	0.284	0.338	0.517		
DS	0.527	0.745	0.906	1.195	1.351	1.598	1.895	2.852		

7 DISCUSSION AND SUMMARY OF RESULTS

7.1 Comparison of results from different methods

This table compares peak flows from various methods with those from the FEH Statistical method at example sites for two key return periods / AEP events. Delete columns which are not required.

		Ratio of peak flow to FEH Statistical peak								
Site code	Return period 2 years / 50% AEP			Return period 100 years / 1% AEP						
oodo	ReFH	ReFH2	Statistical	ReFH	ReFH ReFH2					
East		0.286			0.839					
North		0.105			0.317					
West		0.090			0.284					
DS		0.527	0.444		1.598	1.36				

7.2 Final choice of method

Choice of method and reasons Include reference to type of study, nature of catchment and type of data available.	The statistical mothos is considered more reliable. However the EA model adjut the parameters at the downstream section, therefore such adjustement will be considered to bring more conservative results at the model
How will the flows be applied to a hydraulic model?	Statistical analysis with EA adjustment fitted at the ReFH hydrographs
If relevant. Will model inflows be adjusted to achieve a match with lumped flow estimates, or will the model be allowed to route inflows?	

7.3 Assumptions, limitations and uncertainty

Careful thought should be put into identifying the specific assumptions and limitations applicable to the design peak flow estimates (and design hydrographs). Assessing and reporting on the uncertainty in the estimates is also very important. These sections should be completed for every study and never left blank.

· · ·	
List the main assumptions made (specific to this study)	For the purpose of this study the DS flow with EA adjustment (conservative approach) and ARF for al the subsequent catchments to bring reliable results to the model
Discuss any particular limitations, e.g. applying methods outside the range of catchment types or return periods for which they were developed.	The lack of gauge catchment limitate the possibility of sense check the flow records fo the catchment, however the analysis provided in this report and further FSR provide a robust analysis of the catchment including sensitivity analysis considering downstream water levels and flows.
Provide information on the uncertainty in the design peak flow estimates and the methodology used Uncertainty in the peak flow estimates should always be provided. The default is the 95-percentile upper and lower bounds, but other estimates may need to be provided depending on the requirements of the study. Further information can be found in Section 5.4 of the Flood Estimation Guidelines.	The entire flow peak for the North and West sub -catchmetn has been applied to the upper section of the watercourse in order to provide ston reliable results and accurate flow volumes. Confidence intervals 95% is used in this analysis.
Comment on the suitability of the results for future studies, e.g. at	

nearby locations or for different purposes, would a project for scheme design require additional detail, etc.	
Give any other comments on the study, e.g. suggestions for additional work, such as flow monitoring, rating reviews, etc.	

7.4 Checks

These checks are important as a way of ensuring that everything has been considered and that the results are sensible. All relevant sections should be completed for every study. Where sections are not relevant (where there are no flow gauges or previous studies, for example) a comment should be added to this effect rather than leaving a blank space.

Are the results consistent, for example at confluences? This will not be relevant for a study where there is only a single flow estimation point.	Yes the areas have been calculated with topographic contours and the flow properly calculated with ARF.
What do the results imply regarding the return periods / frequency of floods during the period of record? This will only be relevant where there is flow gauge data.	No gauge is located within this studied catchment
What is the range of 100-year / 1% AEP growth factors? Is this realistic?	DS 3.06 growth factor and yes it is realistic
If 1000-year / 0.1% AEP flows have been derived, what is the range of ratios for 1000-year / 0.1% AEP flow over 100-year / 1% AEP flow?	DS 2.22/1.36=1.63 DS EA factor 6.504/3.53=1.84
How do the results compare with those of other studies? Explain any differences and conclude which results should be preferred. This will not be relevant if there are no previous hydrological assessments.	
Are the results compatible with the longer-term flood history? This will not be relevant if there is no flow gauge data or historical flooding information.	There is no gauge data for the catchment.the modelled flood extent are consistent with hidtorical flood images .
Describe any other checks on the results, e.g. sense-checking hydraulic model results	Sensitivity analysis including robust downstream variations are applied to the flood analysis and model.

7.5 Final results

Show the final results here for all flow estimation points (unless using a distributed approach, with no lumped catchment flow estimation points, and allowing the hydraulic model to route the flows) and design events, and give any other data or results needed for the next stage of the study.

Site code	Flood peak (m³/s) or volumes (m³) for the following return periods (in years)						ls (in			
			<mark>100</mark>	<mark>+15%</mark> CC	<mark>+25%</mark> CC	<mark>+49%</mark> CC	<mark>1000</mark>			
	Floo	od peak	(m³/s) (o <mark>r volu</mark> r	nes (m³) for the	followi	ng AEP	(%) eve	ents
East			<mark>1.868</mark>	<mark>2.48</mark>	<mark>2.335</mark>	<mark>2.783</mark>	<mark>3.441</mark>			
North			<mark>0.991</mark>	<mark>1.139</mark>	<mark>1.238</mark>	<mark>1.476</mark>	<mark>1.825</mark>			
West			<mark>0.671</mark>	<mark>0.772</mark>	<mark>0.839</mark>	<mark>1.000</mark>	<mark>1.237</mark>			
DS EA adjustment			<mark>3.530</mark>	<mark>4.059</mark>	<mark>4.412</mark>	<mark>5.260</mark>	<mark>6.504</mark>			

7.6 Uncertainty bounds

This table reports the flows derived from the uncertainty analysis detailed in Section 7.3. The 'true' value is more likely to be near the estimate reported in Section 7.5 than the bounds. However, it is possible that the 'true' value could still lie outside these bounds.

Complete this table with the flows from the uncertainty analysis. Some key design events have been added to the table, but these can be amended as required.

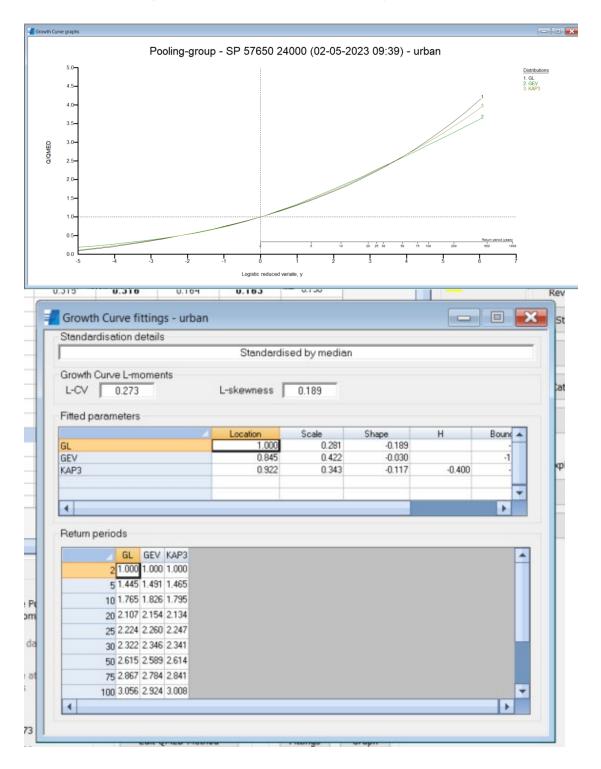
Site code	Flood p	beak (m³/s)	or volumes (m ³) for the following return periods (in years)						
	2		20		100		1,000		
	Flood peak (m³/s) <mark>or volumes (m³)</mark>) for the following AEP (%) events				
	50 5				1	0.1			
	Lower	Upper	Lower	Upper	Lower	Upper	Lower	Upper	
DS	<mark>0.177</mark>	<mark>1.114</mark>	<mark>0.336</mark>	<mark>2.583</mark>	<mark>0.462</mark>	<mark>3.998</mark>	<mark>0.643</mark>	<mark>7.659</mark>	

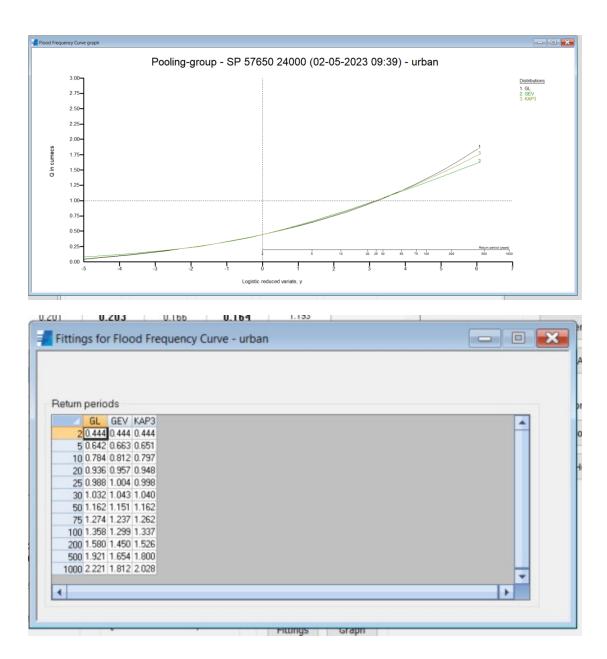
If flood hydrographs are needed for the next stage of the study, where are they provided? (e.g. give filename of spreadsheet,	Flood hydrograph ahas been obtained with ReFH2 statistical analysis with EA
hydraulic model, or reference to table below)	adsjutment applied to obtain robust and better approach of results.

Return period (years)	No dono	or	One don	or	Six don
Confidence level	68%	95%	68%	95%	68%
2	0.63-	0.39-	0.63-	0.40-	0.63-
	1.59	2.54	1.58	2.51	1.59
5	0.61-	0.37-	0.62-	0.38-	0.61-
	1.64	2.68	1.62	2.64	1.63
10	0.60-	0.36-	0.61-	0.37-	0.61-
	1.66	2.75	1.64	2.70	1.64
20	0.60-	0.36-	0.60-	0.36-	0.60-
	1.68	2.82	1.66	2.76	1.66
50	0.59-	0.34-	0.59-	0.35-	0.59-
	1.71	2.91	1.69	2.85	1.68
100	0.58-	0.33-	0.58-	0.34-	0.59-
	1.73	3.01	1.72	2.94	1.71
200	0.57-	0.32-	0.57-	0.33-	0.58-
	1.77	3.13	1.75	3.06	1.74
500	0.55-	0.30-	0.55-	0.31-	0.56-
	1.82	3.33	1.80	3.26	1.79
1000	0.53-	0.28-	0.54-	0.29-	0.54-
	1.88	3.52	1.86	3.45	1.84

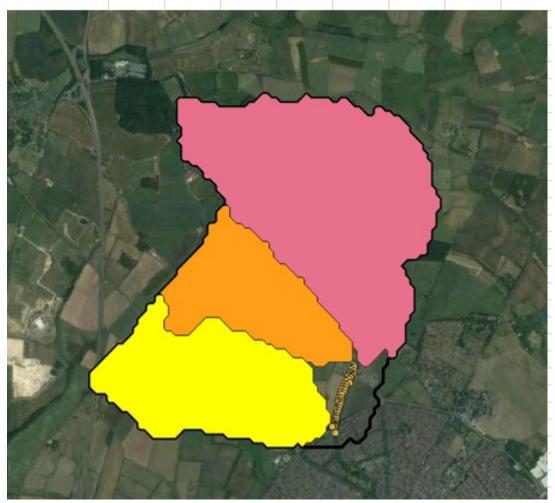
8 ANNEX

Include any additional information which best sits here rather than in the section text, for example, flood peak series, details of historical flood events, rating reviews, pooling groups, or details of flood event analysis. Include important information in the section text, for example, comparison of growth curves, or results of flood event analysis.





				Climate change allownace					
Catchment	Area	%	Q100	15%	25%	49%	Q1000		
Downstream	10.53	100%	1.358	1.562	1.698	2.034	2.221		
West	1.89	17.9%	0.244	0.280	0.305	0.365	0.541		
North	2.79	26.5%	0.360	0.414	0.450	0.539	0.799		
East	5.26	55.6%	0.754	0.868	0.943	1.130	1.676		
		100.0%	0.998	1.148	1.248	1.495	2.217		
	8								



	east	west	north		
	Bis1	Bis2	Bis3		
100	1.868	0.671	0.991		3.530
100+15	2.148	0.772	1.139	Flow calculated from the EA model.	4.059
100+25	2.335	0.839	1.238		4.412
100+49	2.783	1.000	1.476		5.260
1000	3.441	1.237	1.825		6.504